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N91-19221

## Indium Phosphide Solar Cells

I. Weinberg, Chairman  
*NASA Lewis Research Center*  
*Cleveland OH*

The indium phosphide working group considered the following questions.

1. What appears to be the most fruitful directions for InP solar cell research?
2. What can be done to decrease cell cost?
3. What can be done to increase cell efficiency?
4. What measurements are needed for a better understanding of cell performance?
5. n/p vs p/n? Is the question settled? If not what should be done?
6. What is known about SRV?
7. Which areas in radiation effects require additional effort?
8. What are the major problems in cell contacting?
9. Should the present level of InP solar cell research in the U.S.A. be maintained, increased or decreased?

With regard to research directions, the working group recommended continued or additional effort on increasing cell efficiency, reducing cost and the production of larger area cells. Considering the latter it was felt that scale up was not a problem and that high efficiency cells with areas comparable to the present GaAs cells appeared to be feasible.

Suggestions for reducing cell cost included heteroepitaxial growth on cheaper, sturdier substrates such as silicon or germanium, use of processes, such as CLEFT and peeled film technology, which enable one to reuse the presently used, expensive, InP substrate. It was suggested that new crystal growth techniques, to replace the presently used LEC method of crystal growth, could be helpful in reducing substrate cost. With respect to the latter an increase in the number of suppliers, by introducing more competitive pricing, would possibly tend to reduced substrate cost as would the more obvious procedure of procuring large quantities of substrates in a single order. Obviously this would depend on the capability and necessity of producing large quantities of solar cells or on initiation of a Mantech program.

To increase cell efficiency, there is a need for lattice matched window materials in order to reduce the SRV. Semiconductors suggested for this application included AlAsSb and AlInAs with components in the appropriate proportions. The development of multibandgap cells is an obvious direction to take in attaining higher

efficiencies. While this would not necessarily lead to higher efficiencies for InP per se it could result in higher efficiency multicomponent cells, one component of which would be InP. Improved substrate material is a necessity in these efforts. Research directed at higher efficiency should also have as a goal the maintenance of high radiation resistance while at the same time yielding high BOL efficiencies.

Measurements needed for a better understanding of cell performance include absorption coefficients at wavelengths greater than 0.85 micrometers, minority carrier lifetimes, diffusion lengths, SRV and experimental determinations of heavy doping effects. Although there is presently some activity in several of these measurement areas, there is a need for determinations over a wide range of dopant concentrations. Also wherever feasible it would be desirable to perform measurements on the actual solar cell structures.

The question of which configuration is preferable, n/p or p/n, is still undecided. Although several modelling efforts have yielded slightly higher theoretical efficiencies for the p/n configuration, additional experimental results are needed in order to make an intelligent choice. One would have greater confidence in the modelling results if more accurate input parameters were available. It was pointed out that, because of the lower emitter sheet resistance, the n/p configuration was preferable for shallow junction cells. Furthermore, the problem of contacting p-type material needs to be considered in making the final choice. In addition, the few experiments in which both configurations were compared show a slightly lower radiation resistance for the p/n configuration at the higher 1 MeV electron and 10 MeV proton fluences.

Considering surface recombination velocity, there is a need for making this difficult measurement on actual solar cell surfaces. Modelling calculations suggest values approaching  $10^7$  cm/sec for the surface of heavily doped emitters. Although measurements on heavily doped InP, using photoluminescence, indicate values approaching this magnitude there is a need for direct measurements, if feasible, on actual solar cell emitter surfaces. It was pointed out that older measurements, which yielded SRV's in the  $10^3$ - $10^4$  cm/sec range, were obtained on InP which was cleaved in vacuum. Hence, the need for real world measurements.

In the area of radiation effects, there is a need to obtain data over a wide range of energies for both protons and electrons. Additional annealing experiments are required, especially with regard to photon annealing. Flight experiments are a necessity and every effort should be made to seek out and utilize flight opportunities as they arise. Defect studies should be expanded to obtain a more definitive answer to the reasons for the superior radiation resistance of InP.

The working group concluded that InP solar cell research in the US should be at least maintained at its present level and preferably increased. The group surfaced a requirement for increased university participation in the areas of crystal growth, cell fabrication and analysis. In addition to strengthening the present program, this

would result in graduates trained in the special requirements presented by growth of InP crystals and cell processing. In addition the present program would benefit from increased activity in surface passivation and improvements in base substrate material quality.

## Space Cell Theory and Modeling

James Hutchby  
*Research Triangle Institute*  
*Research Triangle Park, NC*

The workshop on PV Theory and Modeling was attended by about thirty people drawn from the industrial, government and academic communities

Discussed during the workshop were current concerns in cell modeling, both general and material-specific, a discussion of PC-1D, a commercial PV modeling computer code, and future issues. The major points discussed at the workshop are displayed in the following viewgraphs.

# **Current Issues in Cell Modeling--GaAs**

## **Physics**

- Anomalous Log I vs V behavior at  $P_{\max}$
- Reverse Bias Breakdown Mechanism(s)
- Dominant Defect Structures Governing Radiation Damage Effects

## **Parameters**

- Minority Carrier Parameters  
(determine directly from minority carrier measurements)

# Current Issues in Cell Modeling--InP

## Physics

- Heavy Doping Effects
  - Bandgap Narrowing
  - Optical Absorption Coefficient
- Anomalously Low  $V_{oc}$  ?
- Surface Recombination

## Parameters

- Many important parameters not well known
  - $n_i, (N_D, N_A)$
  - $L_n, L_p, \tau_n, \tau_p (N_D, N_A)$
  - $S_n, S_p (N_D, N_A, \dots)$

## PC - 1D V.2

### Description

- One-dimensional solar cell model
- Numerical
- Runs on IBM-PC; User-friendly
- Steady-state and transient analysis
- Si, GaAs, AlGaAs built-in models; also user-specified models

### Validation

- Si predictive, GaAs near-predictive

### Issues

- Absorption Coefficient vs. temperature needs more work

## **Future Issues**

### **New problems for modeling**

- **Light-trapping cells**
- **Thin films**



# **Theory and Modeling--Conclusions**

## **GaAs**

- Physics appears to be well understood
- Accurate modeling requires material/process specific parameter measurements
- Radiation induced defects not understood

## **InP**

- Physics needs more work
  - heavy doping effects
  - low  $V_{oc}$
  - surface recombination
- Many important parameters need better measurements

## **Thin films**

- Physics--uncertain
- Parameters--not well known

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## Invited Paper



# Cryogenic Reactant Storage for Lunar Base Regenerative Fuel Cells

Lisa Kohout  
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Cleveland OH*

CRYOGENIC REACTANT STORAGE  
FOR LUNAR BASE REGENERATIVE FUEL CELLS

LISA L. KOHOUT

NASA LEWIS RESEARCH CENTER  
CLEVELAND, OHIO



## POWER TECHNOLOGY DIVISION

**NASA**

### CRYOGENIC REACTANT STORAGE FOR LUNAR BASE REGENERATIVE FUEL CELLS

#### OBJECTIVE

TO DETERMINE THE IMPACT OF CRYOGENIC REACTANT STORAGE ON THE MASS OF AN ALKALINE REGENERATIVE FUEL CELL POWER SYSTEM FOR LUNAR APPLICATION

i.e. DOES STORING THE REACTANT CRYOGENICALLY, INCLUDING A REFRIGERATION PLANT AND EXTRA SOLAR ARRAY TO POWER IT, RESULT IN A LOWER OVERALL SYSTEM MASS THAN CONVENTIONAL PRESSURIZED GAS STORAGE?

THE CARROT: CRYOGENIC STORAGE TAKES MUCH LESS TANK WEIGHT PER POUND OF REACTANT THAN GASEOUS STORAGE

THE STICK: CRYOGENIC STORAGE REQUIRES A REFRIGERATION PLANT AND EXTRA POWER



## **POWER TECHNOLOGY DIVISION**



### **CRYOGENIC REACTANT STORAGE FOR LUNAR BASE REGENERATIVE FUEL CELLS**

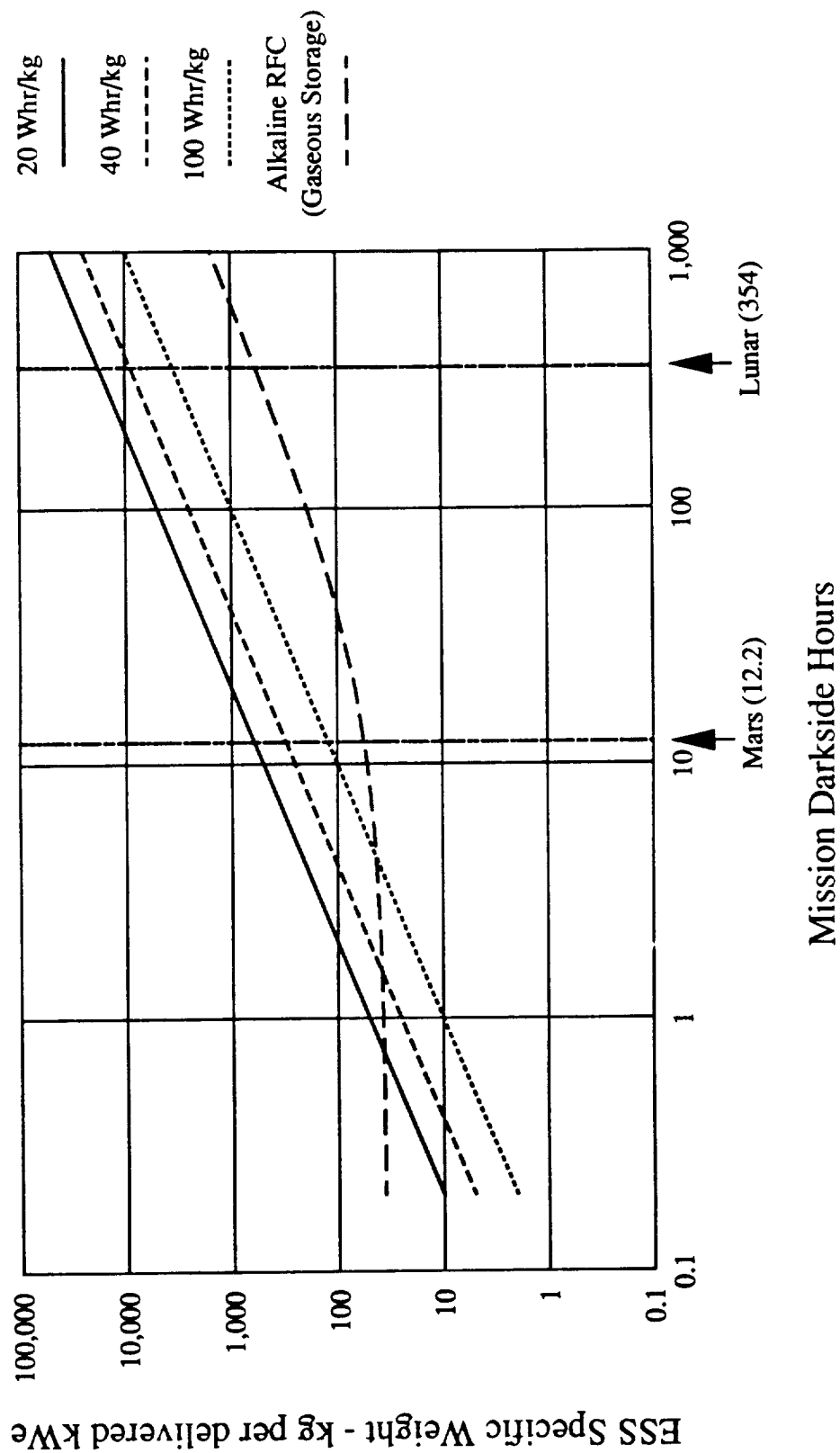
#### **APPROACH**

**MODEL A CONVENTIONAL RFC POWER SYSTEM FOR A  
MANNED LUNAR INSTALLATION**

**REPLACE THE GASEOUS HYDROGEN AND OXYGEN STORAGE  
TANKS WITH LIQUEFACTION UNITS AND CRYOGENIC  
STORAGE TANKS**

**CONSIDER 20 kW AND 250 kW SYSTEMS**

# RFC vs. Batteries for Varied Darkside Periods



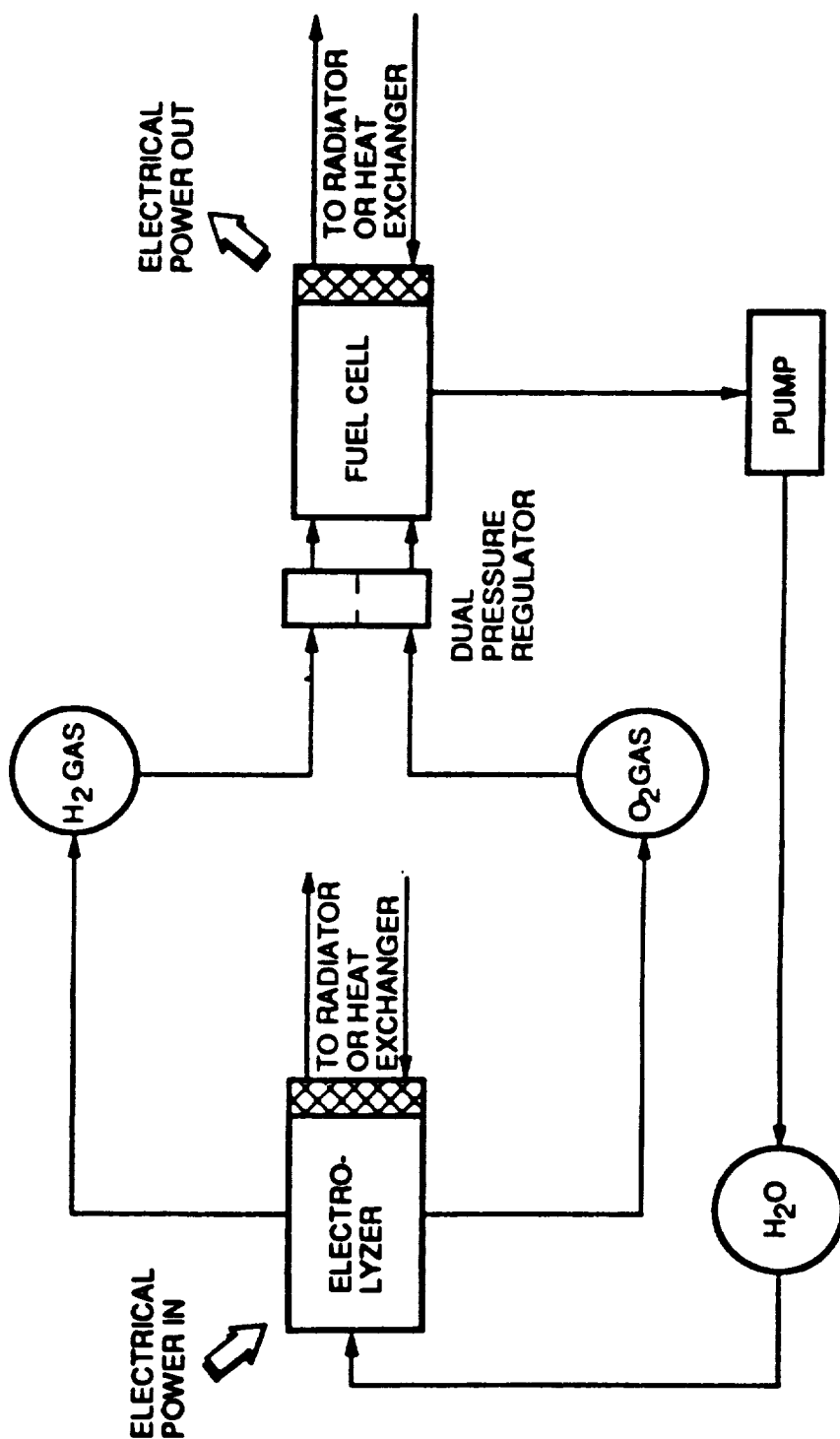




## POWER TECHNOLOGY DIVISION



### CONVENTIONAL REGENERATIVE FUEL CELL SYSTEM (REACTANTS STORED AS PRESSURIZED GASES)

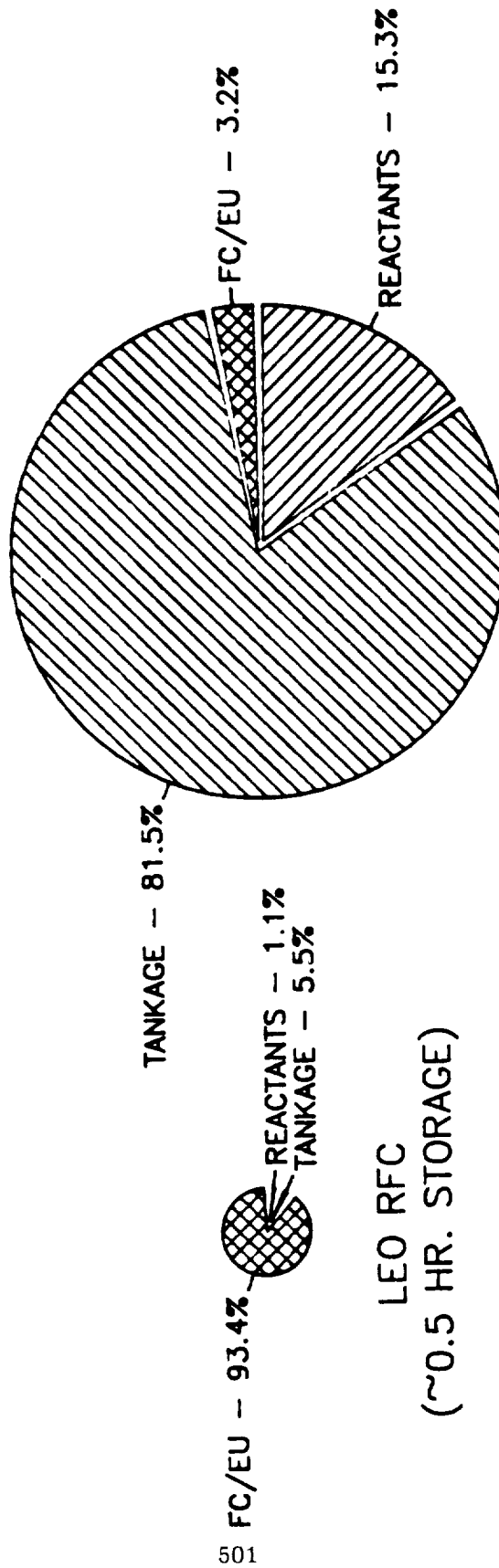




## POWER TECHNOLOGY DIVISION



### COMPARISON OF MASS BREAKDOWNS FOR A 250 kW REGENERATIVE FUEL CELL SYSTEM



(INCONEL TANK MATERIAL)

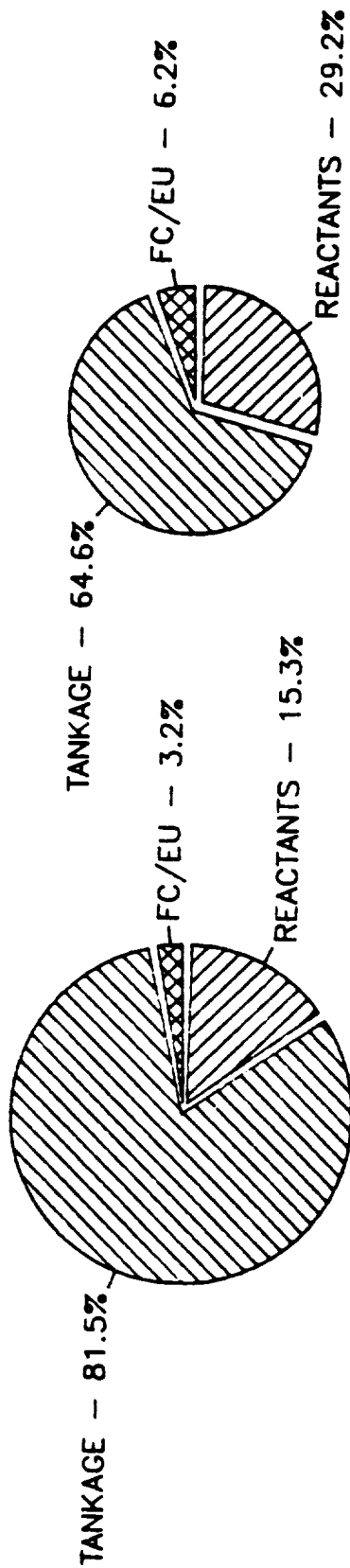
LUNAR RFC  
(~330 HR. STORAGE)



## POWER TECHNOLOGY DIVISION



### MASS BREAKDOWN FOR A 250 kW LUNAR REGENERATIVE FUEL CELL SYSTEM



INCONEL TANKS

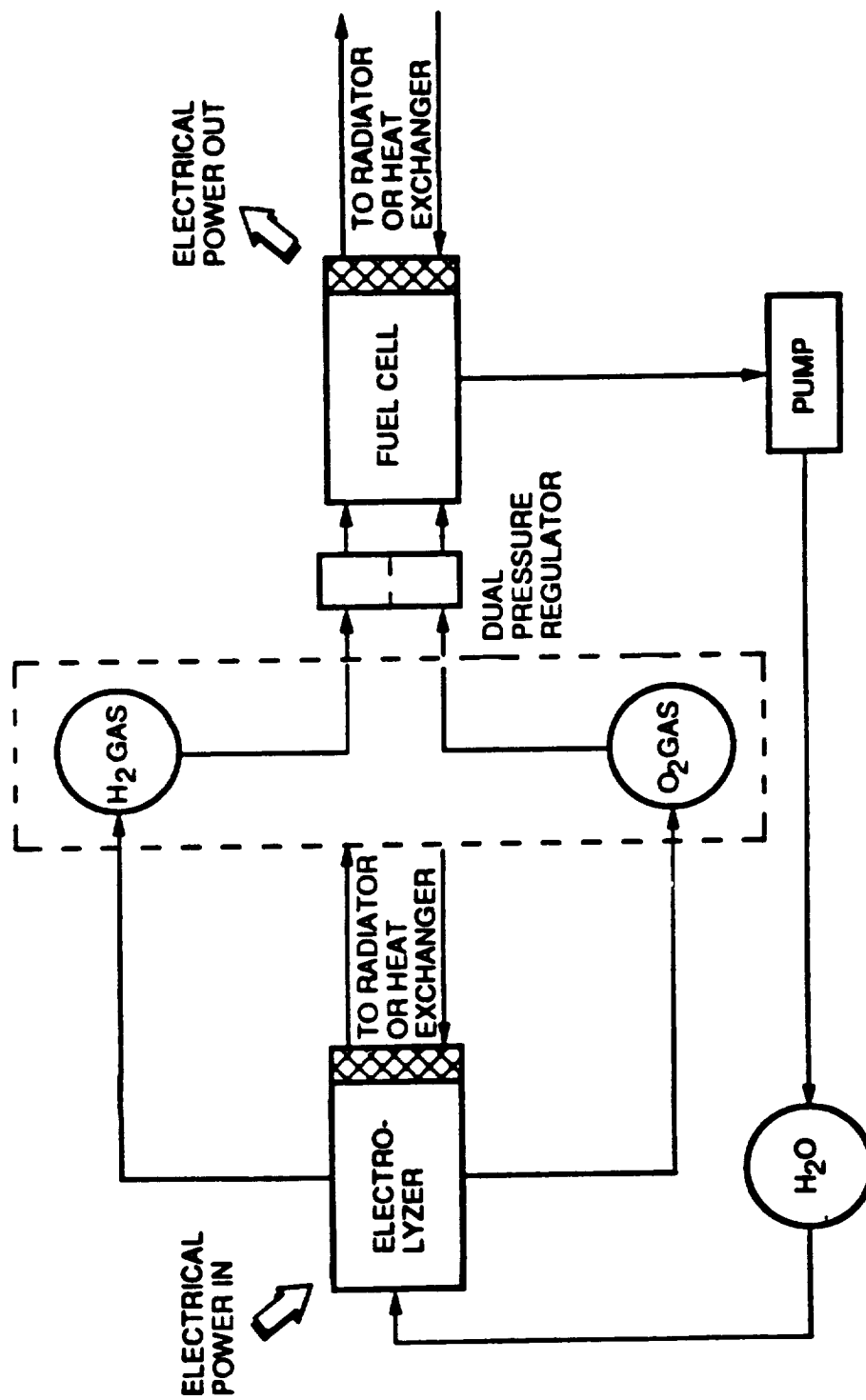
KEVLAR TANKS



## POWER TECHNOLOGY DIVISION



### CONVENTIONAL REGENERATIVE FUEL CELL SYSTEM (REACTANTS STORED AS PRESSURIZED GASES)

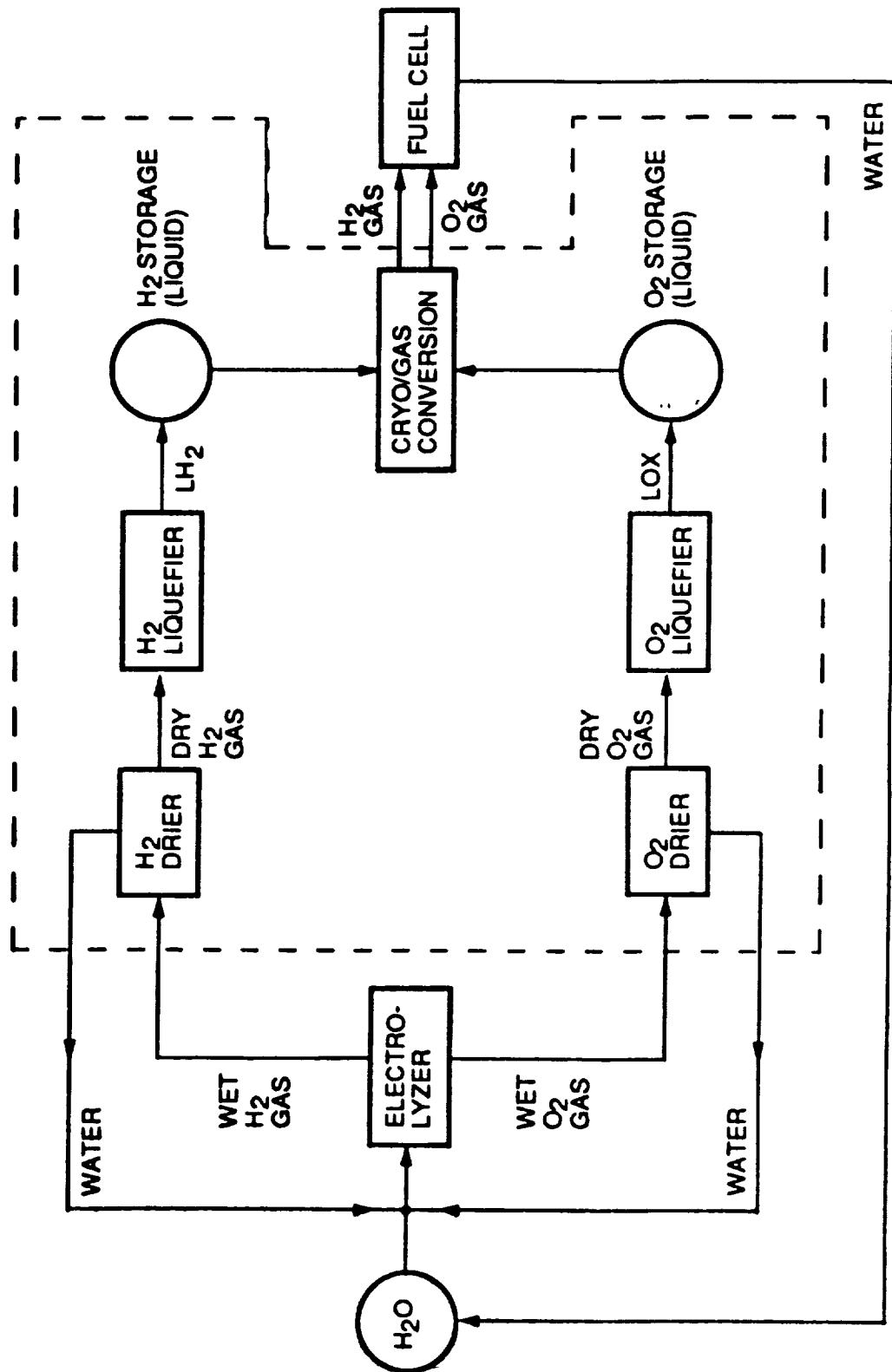




## POWER TECHNOLOGY DIVISION



### REGENERATIVE FUEL CELL SYSTEM (REACTANTS STORED AS CRYOGENIC FLUIDS)





## POWER TECHNOLOGY DIVISION NASA

### MODELING OF FUEL CELL / ELECTROLYZER SUBSYSTEM

0 MODELED USING CODE DEVELOPED AT NASA LEWIS  
BY M. HOBerecht AND L. RIEKER

0 OPERATING CONDITIONS

#### FUEL CELL

CELL ACTIVE AREA	930 SQ.CM.
OPERATING TEMPERATURE	355 K
OPERATING PRESSURE	0.4 MPa
CURRENT DENSITY	161 mA/SQ.CM.

#### ELECTROLYZER

CELL ACTIVE AREA	930 SQ.CM.
OPERATING TEMPERATURE	355 K
OPERATING PRESSURE	2.2 MPa
CURRENT DENSITY	161 mA/SQ.CM.



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### MODELING OF DRYING AND LIQUEFACTION SUBSYSTEMS

PRIMARY REFERENCE FOR PRODUCTION OF CRYOGENS IN SPACE:

"IN-SPACE PROPELLANT PROCESSING USING WATER DELIVERED AS SHUTTLE CONTINGENCY PAYLOAD," E.H. BOCK AND J.G. FISHER, GENERAL DYNAMICS CONVAIR DIVISION, 1978.

#### SCENARIO

- 0 SHUTTLE DELIVERS WATER STORED AS CONTINGENCY PAYLOAD TO ON-ORBIT PROPELLANT PROCESSING FACILITY
- 0 AT PROCESSING FACILITY, WATER IS ELECTROLYZED AND PRODUCT GASES LIQUEFIED AND STORED AS CRYOGENS
- 0 CRYOGENS USED AS PROPELLANTS FOR SPACE-BASED OTV

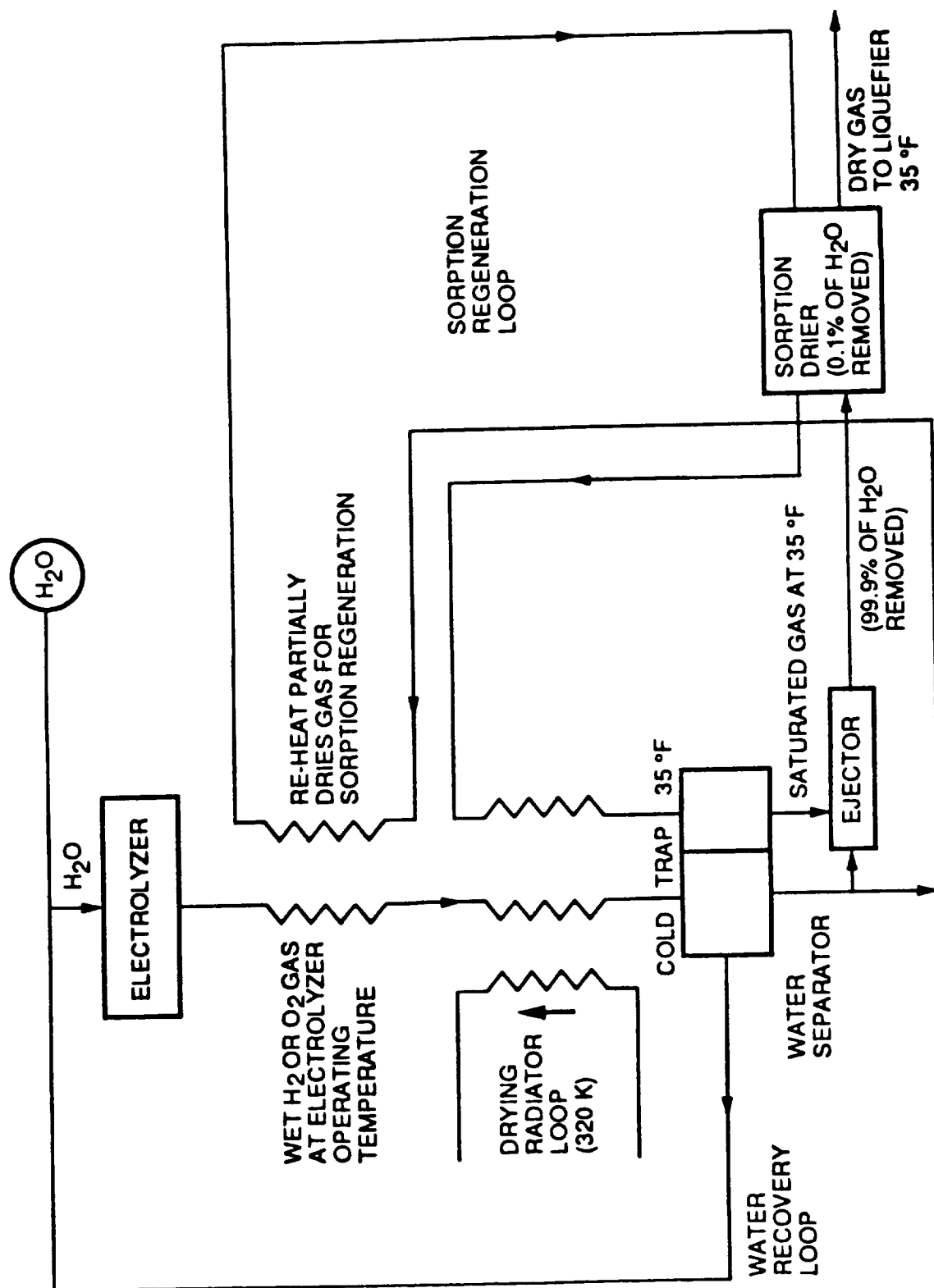
REFERENCE DESCRIBES THE DEFINITION AND PRELIMINARY DESIGN OF THE PROPELLANT PROCESSOR SUBSYSTEMS INCLUDING DRYING, LIQUEFACTION, AND STORAGE



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## GASEOUS HYDROGEN/OXYGEN DRYING SYSTEM







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### MODELING OF HYDROGEN/OXYGEN LIQUEFACTION SYSTEM

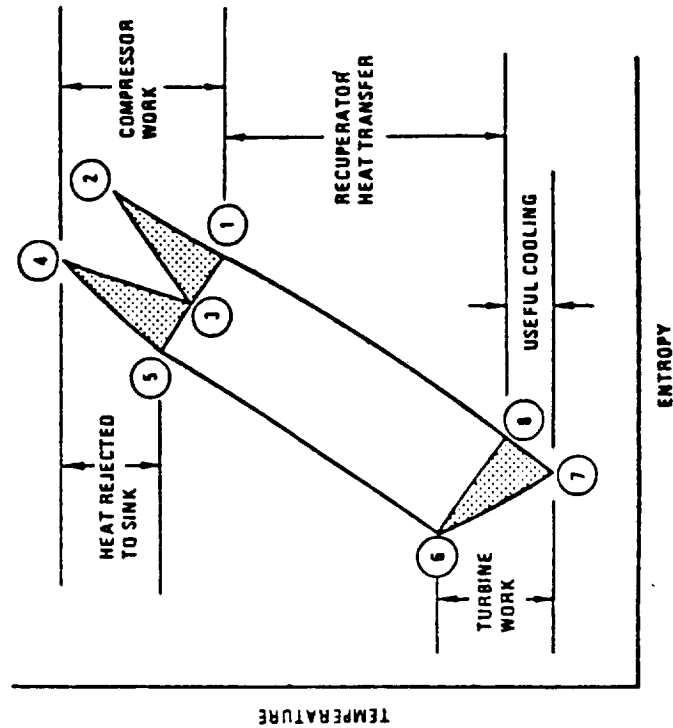
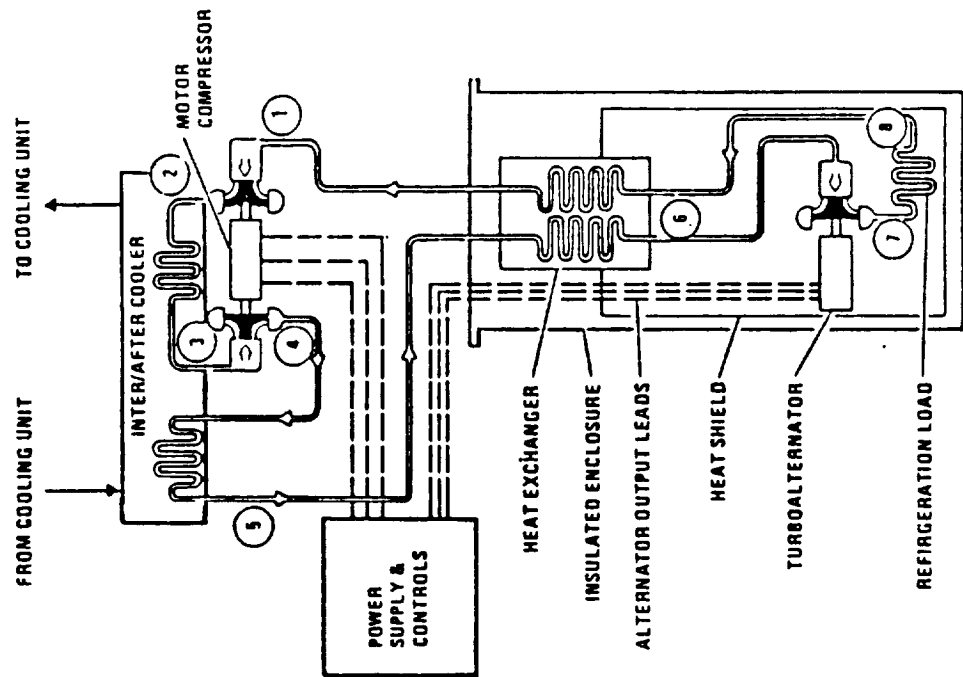
- 0 UTILIZES REVERSED BRAYTON CYCLE FOR LIQUEFACTION
- 0 LIQUEFIES H<sub>2</sub>/O<sub>2</sub> GAS AS WELL AS BOIL-OFF FROM STORAGE TANKS
- 0 EQUIPMENT REQUIRED FOR HYDROGEN AND OXYGEN LIQUEFACTION IS SIMILAR EXCEPT THAT TWO REFRIGERATION STAGES ARE REQUIRED FOR HYDROGEN



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## REVERSED BRAYTON LIQUEFACTION CYCLE



REFRIGERATION CYCLE



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### MODELING OF CRYOGENIC REACTANT STORAGE TANKS

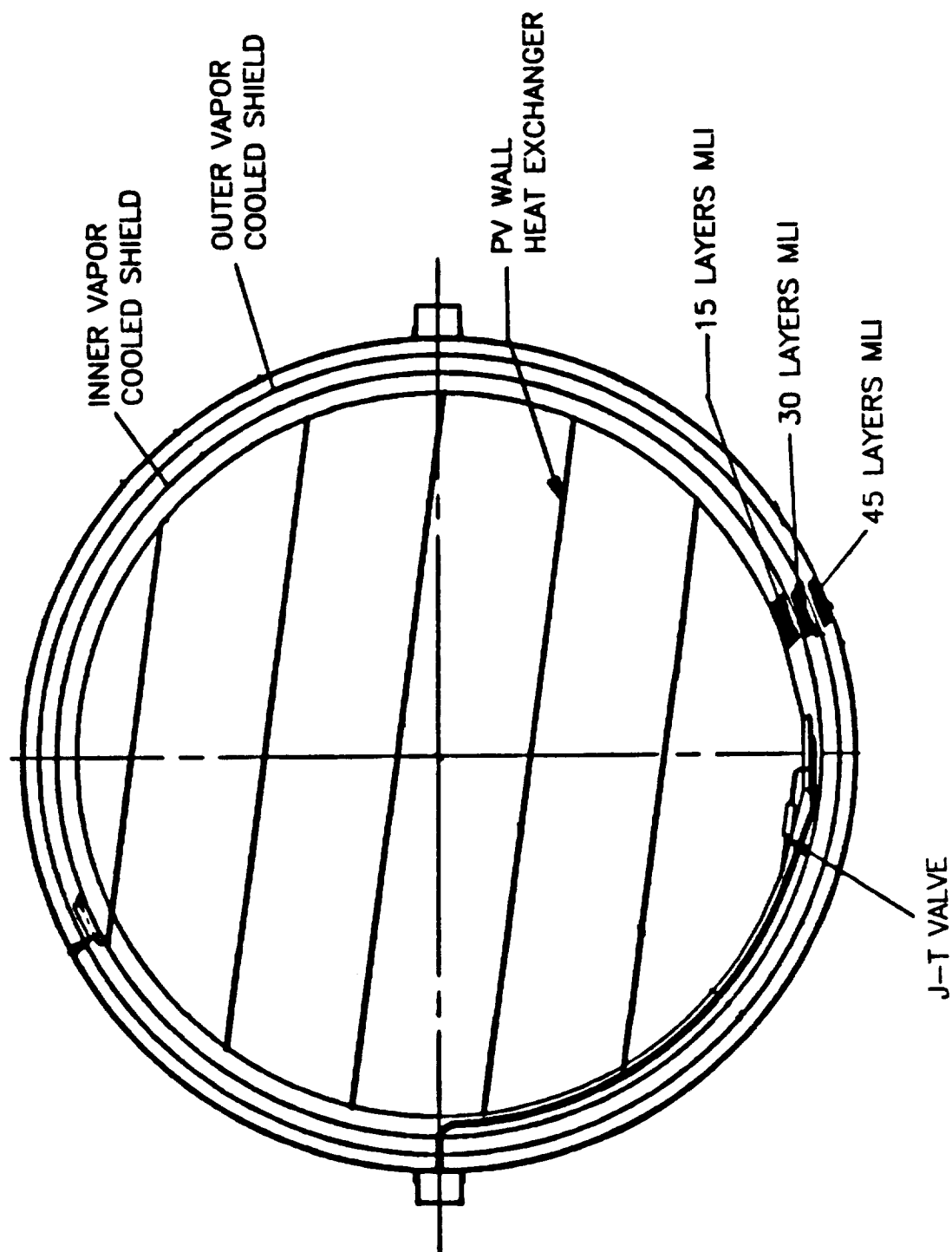
- 0 BASED ON BEECHCRAFT DESIGN  
SPACE STATION EXPERIMENT DEFINITION:  
LONG-TERM CRYOGENIC FLUID STORAGE
- 0 ALUMINUM INNER PRESSURE VESSEL AND OUTER SHELL
- 0 90 LAYERS OF MULTILAYER INSULATION AND 2 VAPOR COOLED  
SHIELDS PLACED BETWEEN CONCENTRIC INNER AND OUTER  
SHELLS
- 0 5% REACTANT RESIDUAL ALLOWED
- 0 ADDITIONAL 10% TANK VOLUME ALLOWED TO ACCOMMODATE  
MAXIMUM ACHIEVABLE FILL LEVEL



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### SCHEMATIC OF CRYOGENIC STORAGE TANK





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### MODELING OF SUBSYSTEM RADIATORS

0 RADIATORS ARE REQUIRED FOR THE FOLLOWING SUBSYSTEMS:

FUEL CELL

DRYING

OXYGEN LIQUEFACTION

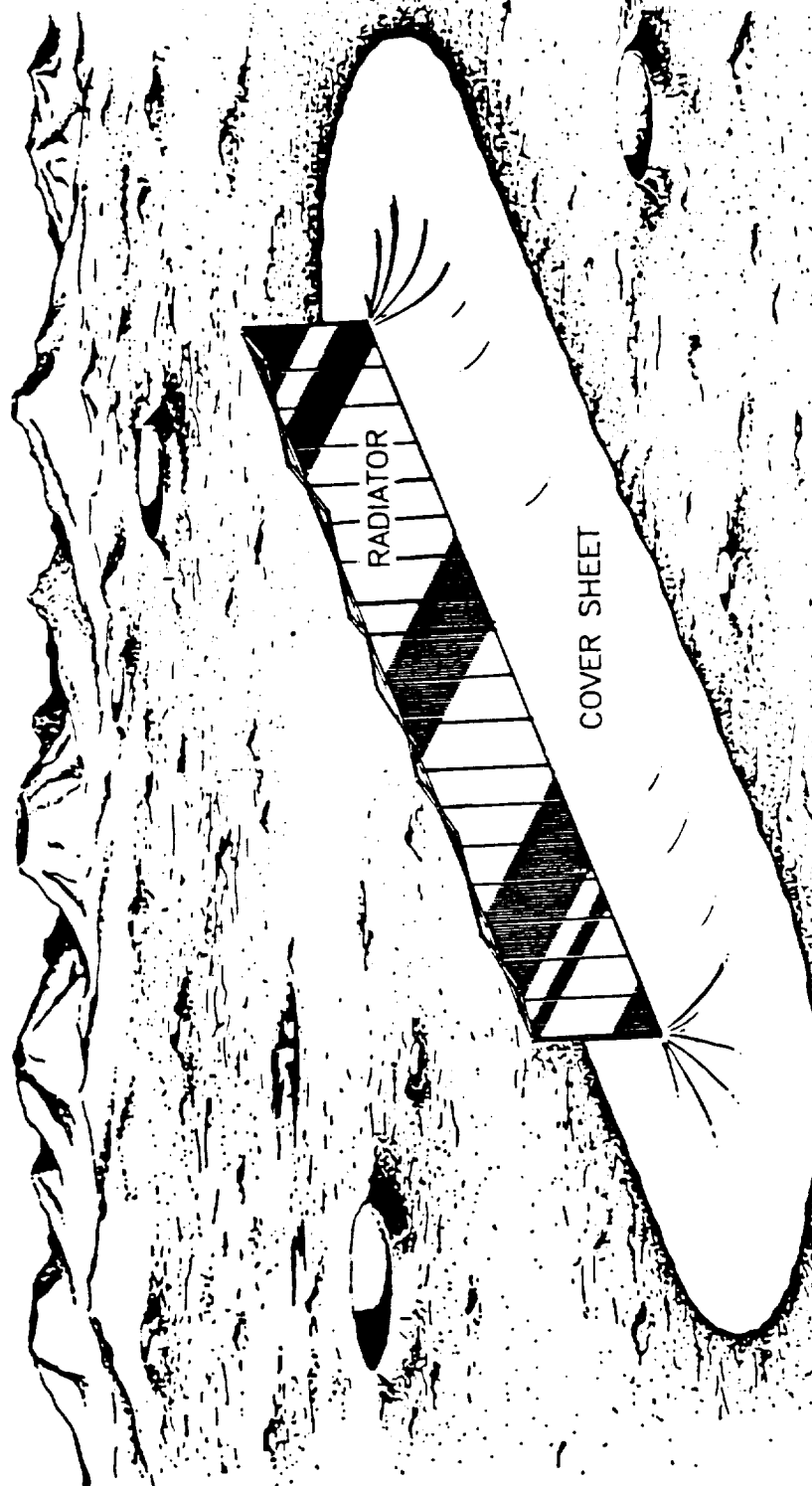
HYDROGEN LIQUEFACTION

0 ALL RADIATORS EXCEPT FUEL CELL RADIATOR WERE SIZED BASED ON REJECTION TEMPERATURES AND APPROXIMATED HEAT LOADS FROM BOCK AND FISHER REFERENCE

0 FUEL CELL RADIATOR WAS SIZED BASED ON REJECTION TEMPERATURE AND HEAT LOAD FOUND FROM RFC CODE

0 DAYTIME SINK TEMPERATURE OF 220 DEG K WAS USED (VERTICAL ORIENTATION OVER SURFACE SHEET)

# SCHEMATIC OF RADIATOR WITH GROUND COVER SHEET



REFERENCE: "A METHOD FOR REDUCING THE EQUIVALENT SINK TEMPERATURE OF A VERTICALLY ORIENTED RADIATOR ON THE LUNAR SURFACE",  
D. BIEN AND D. GUENTERT, NASA LERC, 1968



## POWER TECHNOLOGY DIVISION NASA

### MODELING OF SOLAR PHOTOVOLTAIC ARRAY

- 0 GaAs SUN-TRACKING ARRAY ON LUNAR SURFACE
  - INCLUDES ARRAY BLANKET, SUPPORT FRAME, PIVOTS, TRACKING MOUNT, AND WIRING HARNESS

EFFICIENCY

22.512 %

SPECIFIC POWER<sup>\*</sup>

123 W/KG

SPECIFIC MASS

2.48 KG/SQ.M.

\* (@ 22.512% EFFICIENCY, 110 DEG.C.)



# POWER TECHNOLOGY DIVISION NASA

## BREAKDOWN OF POWER REQUIREMENTS 250 kW SYSTEM

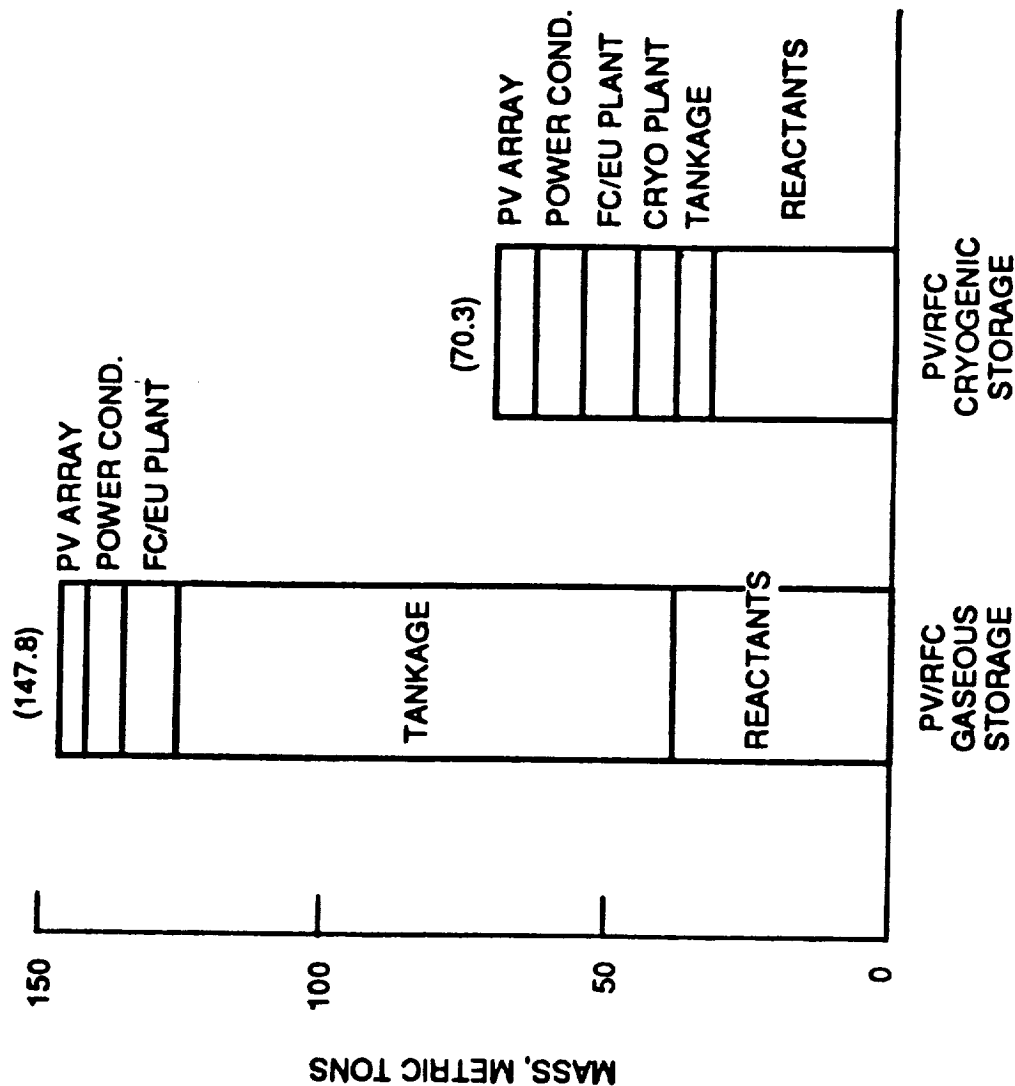
COMPONENT	POWER TO BE SUPPLIED BY PV ARRAY (kW)
ELECTROLYZER	400.0
H2/O2 DRIERS	2.0
H2 LIQUEFACTION UNIT	123.5
O2 LIQUEFACTION UNIT	71.3
BASELINE POWER TO USER	250.0
TOTAL POWER TO BE DELIVERED BY PV ARRAY:	846.8
REQUIRED ARRAY AREA:	2780 SQ.M. (2134 SQ.M. W/O CRYO STORAGE)





# POWER TECHNOLOGY DIVISION NASA

## 250 kW LUNAR SURFACE POWER SYSTEM COMPARISON





## POWER TECHNOLOGY DIVISION



### COMPARISON OF REACTANT STORAGE TANK SIZES 250 kW SYSTEM

	GASEOUS STORAGE (KEVLAR)	CRYOGENIC STORAGE
HYDROGEN TANK		
MASS OF H <sub>2</sub> (M.T.)	4.40	3.59
RADIUS (M)	9.0	INNER SHELL: 2.4 OUTER SHELL: 2.6
VOLUME (CU.M.)	2969	56
OXYGEN TANK		
MASS OF O <sub>2</sub> (M.T.)	34.9	28.5
RADIUS (M)	7.1	INNER SHELL: 1.9 OUTER SHELL: 2.0
VOLUME (CU.M.)	1485	27

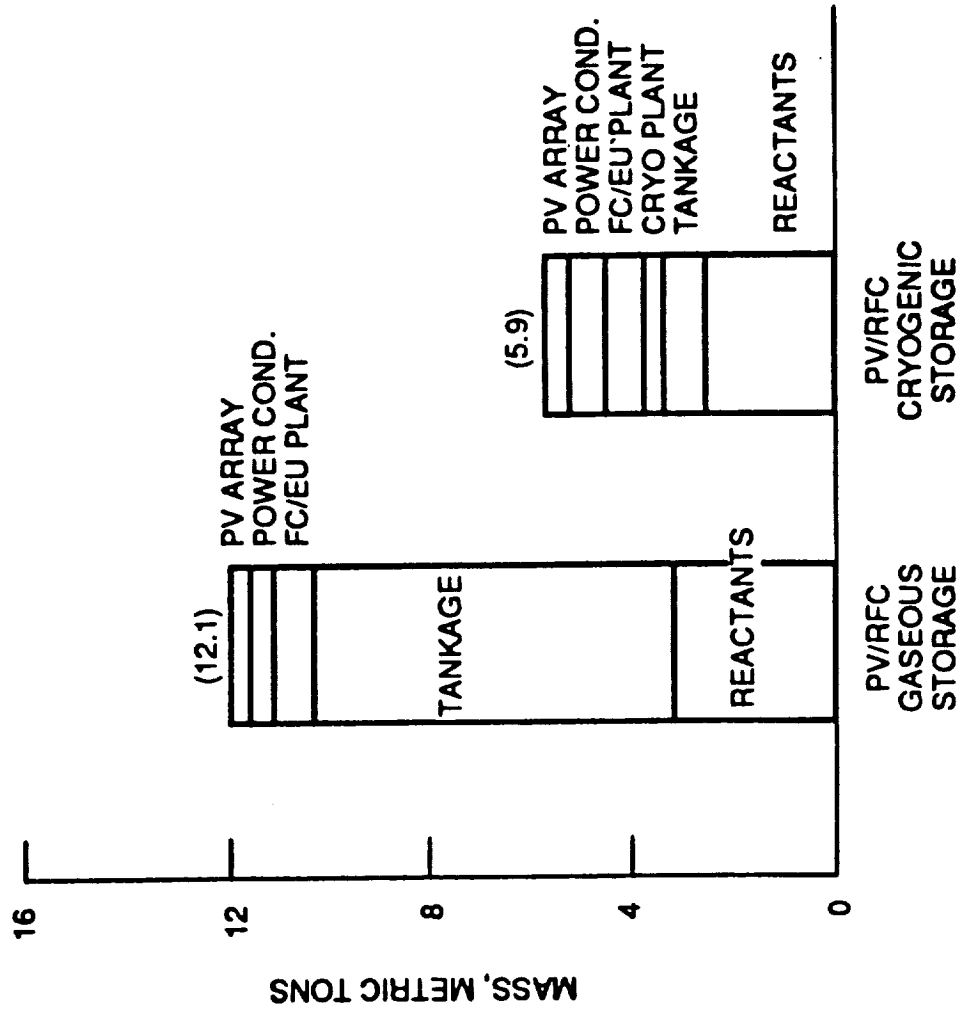
(BASED ON SINGLE TANK PER REACTANT)



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### 20 kW LUNAR SURFACE POWER SYSTEM COMPARISON





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### CONCLUSIONS

- 0 CRYOGENIC REACTANT STORAGE APPEARS TO HAVE A MAJOR BENEFIT FOR LUNAR SURFACE REGENERATIVE FUEL CELL ENERGY STORAGE SYSTEMS
- 0 REDUCTION IN TANK WEIGHT MORE THAN COMPENSATES FOR THE ADDITIONAL WEIGHT OF LIQUEFACTION PLANTS, RADIATORS, AND PV ARRAYS
- 0 FOR SOLAR PV/RFC POWER SYSTEMS UTILIZING CRYOGENIC STORAGE, THE RESULTING OVERALL MASS REDUCTION IS APPROXIMATELY 50 PERCENT (COMPARED WITH GAS STORAGE USING FILAMENT WOUND PRESSURE VESSELS)
- 0 SYNERGISTIC USER BENEFITS ALSO EXIST - THE CRYO RFC SYSTEM CAN PROVIDE LOX AND LH2 ON-SITE FOR OTHER USES (REFUELING, PROPELLANTS, ETC.)



## **POWER TECHNOLOGY DIVISION      NASA**

### **AREAS FOR FURTHER STUDY**

- 0   SCALABILITY OF THE LIQUEFACTION PROCESS COMPONENTS**
- 0   OPTIMIZATION OF SUBSYSTEMS**
- 0   CRYOGEN-FUEL CELL INTERFACE**
- 0   INFRASTRUCTURE CONSIDERATIONS**
- 0   RELIABILITY/REDUNDANCY TRADE-OFFS**